

# **USE OF CARBON FIBER COMPOSITE MOLECULAR SIEVES FOR AIR SEPARATION**

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SEPARATION**

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## ABBREVIATIONS

### Terms

BET	Brunauer, Emmett, and Teller (theory) [14]
CFCMS	carbon fiber carbon molecular sieve
ESA	electrical swing adsorption
IGA	Intelligent Gas Analyzer (Hidden Instruments term)
ORNL	Oak Ridge National Laboratory
PSA	pressure swing adsorption
SEM	scanning electron microscopy

### Gases

CO <sub>2</sub>	carbon dioxide
N <sub>2</sub>	nitrogen
O <sub>2</sub>	oxygen

### Units

Bar	barometric pressure ( $\equiv$ 0.1 MPa or 1.01325 atmospheres)
°C	degrees Celsius
K	degrees Kelvin
MPa	megapascal
m <sup>2</sup> /g <sup>-1</sup>	square meters per gram
mbar/min	millibar of pressure per minute
mg/min	milligram per minute
nm	nanometer
%	percent
wt%	weight percent (% of mass)



# **USE OF CARBON FIBER COMPOSITE MOLECULAR SIEVES FOR AIR SEPARATION**

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## **EXECUTIVE SUMMARY**

A novel adsorbent material, “carbon fiber composite molecular sieve” (CFCMS), has been developed by the Oak Ridge National Laboratory. Its features include high surface area, large pore volume, and a rigid, permeable carbon structure that exhibits significant electrical conductivity. The unique combination of high adsorptive capacity, permeability, good mechanical properties, and electrical conductivity represents an enabling technology for the development of novel gas separation and purification systems. In this context, it is proposed that a fast-cycle air separation process that exploits a kinetic separation of oxygen and nitrogen should be possible using a CFCMS material coupled with electrical swing adsorption (ESA).

The adsorption of O<sub>2</sub>, N<sub>2</sub>, and CO<sub>2</sub> on activated carbon fibers was investigated using static and dynamic techniques. Molecular sieving effects in the activated carbon fiber were highlighted by the adsorption of CO<sub>2</sub>, a more sensitive probe molecule for the presence of microporosity in adsorbents. The kinetic studies revealed that O<sub>2</sub> was more rapidly adsorbed on the carbon fiber than N<sub>2</sub>, and with higher uptake under equilibrium conditions, providing the fiber contained a high proportion of very narrow micropores. The work indicated that CFCMS is capable of separating O<sub>2</sub> and N<sub>2</sub> from air on the basis of the different diffusion rates of the two molecules in the micropore network of the activated carbon fibers comprising the composite material.

In response to recent enquires from several potential users of CFCMS materials, attention has been given to the development of a viable continuous process for the commercial production of CFCMS material. As part of this effort, work was implemented on characterizing the performance of lignin-based activated carbon fiber, a potentially lower cost fiber than the pitch-based fibers used for CFCMS production to date. Similarly, to address engineering issues, measurements were made to characterize the pressure drop of CFCMS as a function of carbon fiber dimensions and monolith density.

## **1.1 INTRODUCTION**

A novel adsorbent material, carbon fiber composite molecular sieve (CFCMS), has been developed by the Oak Ridge National Laboratory (ORNL) [1-3]. Upon thermal activation, usually in CO<sub>2</sub> or steam, the carbon fiber-based material develops a large micropore volume (0.5-1.0 cm<sup>3</sup>/g) and high BET surface area (1000-2200 m<sup>2</sup>/g). As shown in the scanning electron microscopy (SEM) image in Figure 1, the structure of CFCMS comprises carbon fibers, ~10 μm in diameter, bonded at their contact points to provide a continuous carbon skeleton that is electrically conductive. The structure is open and permeable, which allows fluids to readily flow



through the material with minimal pressure drop. The unique combination of the open structure, microporosity, and electrical conductivity allows the material to be used in a regenerative, electrical swing adsorption (ESA) system [4-6].

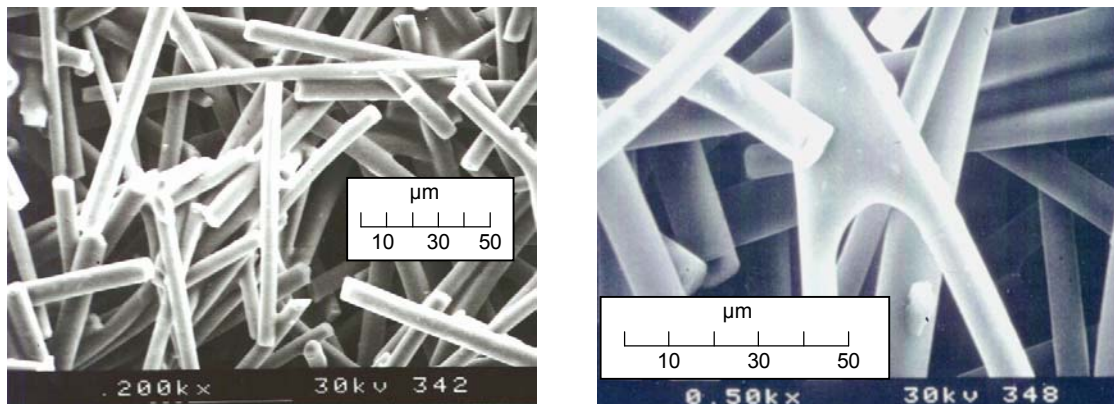


Figure 1 - SEM images showing the structure of CFCMS material

In essence, ESA is an electrical analog of pressure swing adsorption (PSA), whereby desorption of the adsorbate is facilitated by the passage of an electric current through the adsorbent to obtain resistive heating [5, 6]. In this context, CFCMS represents an enabling technology for an ESA process in which efficient desorption could be achieved in the absence of pressure swings. The bottom line is that significant energy savings could be realized because the adsorption beds do not, in principle, require repressurization after each desorption step. This is consistent with the viewpoint of Jasra et al. [7], who in a review of the separation of gases by PSA noted that "although there is some room for improvement in the PSA process, the potential gains in process economics in the future are likely to come from the development of new and improved adsorbents".

CFCMS composites are produced using the process illustrated in Figure 2. Using a purpose-built vacuum slurry molding apparatus at ORNL, isotropic pitch-based carbon fibers are blended with a powdered phenolic resin at a typical ratio of four parts fiber to one part resin (by weight) in water. The dilute slurry is molded in a process somewhat similar to the forming of a pulp fiber mat in a papermaking process [2, 3]. After molding, the green CFCMS composites are dried at ~50°C for 24 hours and then heated to about 130°C for a further 24 hours to cure the phenolic resin. If a high bulk density material is required, the dried form is hot-pressed at a temperature of about 300°C prior to carbonization. The dried (or hot-pressed) composites are carbonized in a nitrogen atmosphere at 650°C for 4 hours, followed by thermal activation in a CO<sub>2</sub> or steam atmosphere at 850°C until the desired level of carbon burn-off, i.e., activation, is attained (as measured by weight loss). The activated composite material is then machined to the desired final shape and dimensions.

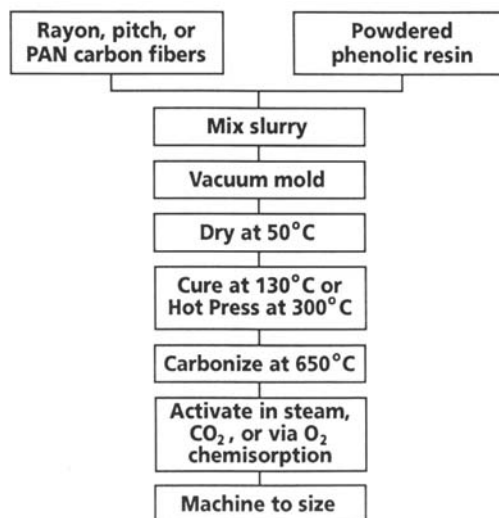


Figure 2 - The major processing operations in the fabrication of CFCMS composite [1-3]

Preliminary work demonstrated that CFCMS material has the potential for separating O<sub>2</sub> and N<sub>2</sub> in air [8-10]. However, the findings also indicated that a more efficient separation could be obtained if the micropore size distribution of the activated carbon fiber component could be better tailored for this purpose. Therefore, to provide the foundation for developing a suitable CFCMS material, a series of isotropic pitch-based activated carbon fiber products was prepared in which the degree of activation of the fiber was varied in the range of 5-30% (carbon burn-off). The pore size distributions of these products were characterized, and correlated with the kinetics of adsorption of O<sub>2</sub> and N<sub>2</sub>, respectively, on the activated carbon fibers. The findings are summarized here.

## 1.2 EXPERIMENTAL

### 1.2.1 Materials Preparation

On a Hiden Analytical “Intelligent Gravimetric Analyzer” (IGA) instrument (Figure 3), 140 mg samples of isotropic pitch-based carbon fibers (Anshan East Asia Carbon Co.) were activated to the desired level of carbon burn-off, as measured by weight loss, at a temperature of 835°C in an atmosphere of pure CO<sub>2</sub> (at ambient pressure).

### 1.2.2 Materials Characterization

The surface area and pore size distribution of representative samples of the activated carbon fibers were characterized by nitrogen adsorption at 77K (-196°C) and CO<sub>2</sub> adsorption at 273K (0°C) using a Quantachrome Autosorb-1 instrument. Apparent surface areas were derived from the N<sub>2</sub> and CO<sub>2</sub> adsorption isotherms using the standard BET method [11, 12]. Pore size distributions were calculated from the adsorption data by application of the density functional theory (DFT) approach [13, 14]. Similarly, micropore volumes were estimated using the Dubinin-Astakov (DA) equation [12].

### 1.2.3 Kinetic Studies

Using the Hiden IGA instrument (Figure 3), dynamic measurements were made on the activated carbon fiber products, in which the adsorption of  $O_2$  and  $N_2$ , respectively, was monitored as a function of time to examine the approach to equilibrium, during and after a constant-rate pressure rise from 0.001 to 0.1 MPa (0.01 to 1 bar). This pressure range was selected because the isotherms shown in Figure 4 for  $O_2$  and  $N_2$  adsorption at 294K on a CFCMS material (10% burn-off level) are steepest at low pressure, and therefore kinetic effects should be more easily observed [8-10].

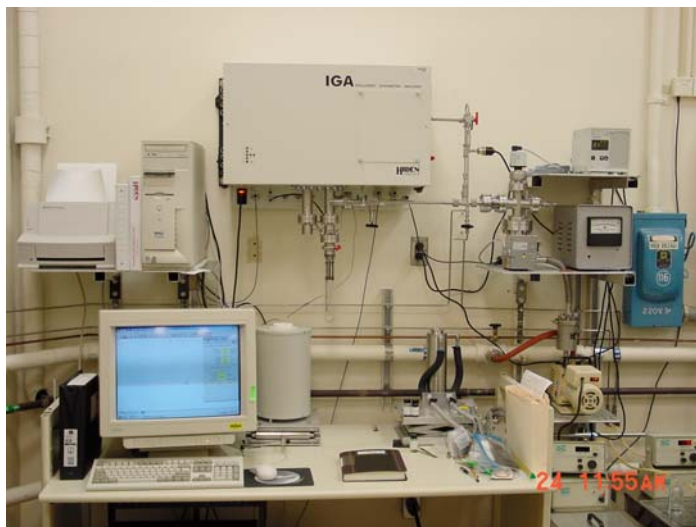


Figure 3 - Hiden IGA Instrument

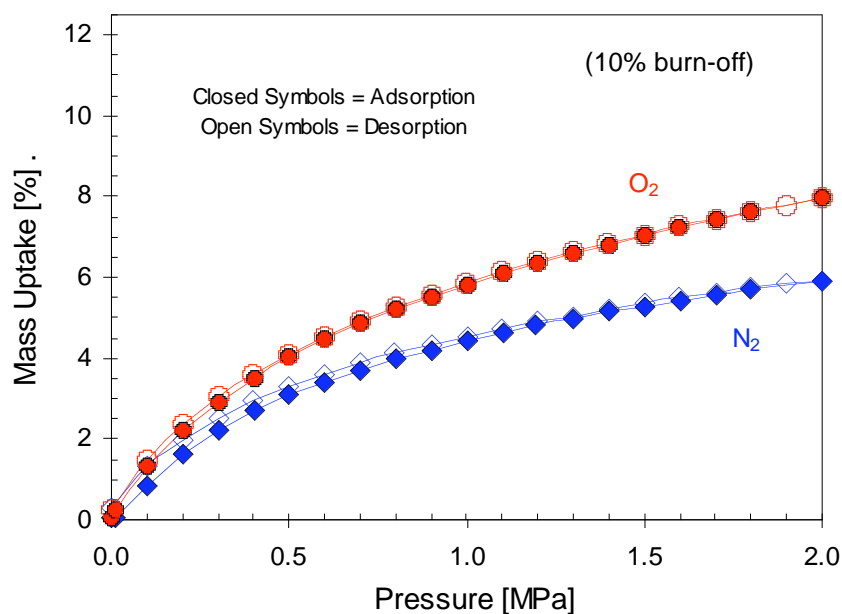


Figure 4 - High pressure  $O_2$  and  $N_2$  isotherms on CFCMS at 294K

The activated carbon fiber samples were outgassed under high vacuum ( $< 10^{-10}$  MPa, or  $10^{-9}$  bar) at a temperature of 300°C immediately before the kinetic measurements of O<sub>2</sub> and N<sub>2</sub> adsorption.

## 1.3 RESULTS AND DISCUSSION

### 1.3.1 Summary of Preliminary Findings

In the preliminary work reported earlier [8-10], adsorption isotherms of pure O<sub>2</sub> and N<sub>2</sub>, respectively, were determined on two CFCMS materials (carbon burn-off levels of 10 and 26%, respectively) over a pressure range of 0-2 MPa (0-20 bar), at temperatures of 294K (21°C), 338K (65°C), and 358K (85°C). In keeping with the thermodynamics of adsorption, equilibrium uptake of each gas decreased with increasing temperature. Furthermore, on either a mass or molar basis, the equilibrium uptake of O<sub>2</sub> on the CFCMS materials was greater than that of N<sub>2</sub> (at each temperature). This is exemplified in Figure 4 above for O<sub>2</sub> and N<sub>2</sub> adsorption at 294K on the CFCMS material with a carbon burn-off level of 10%. At a pressure of 2 MPa, the uptakes of O<sub>2</sub> and N<sub>2</sub> on the CFCMS material were ~8 and ~6 wt%, respectively.

The low-pressure hysteresis exhibited by the N<sub>2</sub> isotherm in Figure 4 is unusual, and may possibly be an artifact of the method of measurement. That is, even though the measurements were continuously made over almost two days, insufficient time was allowed for establishment of equilibrium during determination of the desorption isotherm at lower pressures. As is common practice in using computer-controlled instruments for gas adsorption measurements, a constant value for the “time-out” function was entered into the operating parameters of the IGA instrument; i.e., the elapsed time at which the IGA moves onto the determination of the next isotherm point regardless of whether it is still detecting a change in sample mass. A post-mortem of the IGA data obtained in the preliminary work revealed that all the low pressure desorption points shown in Figure 4 for N<sub>2</sub> adsorption on the CFCMS material were, in fact, based on mass values recorded when the time-out point at a given pressure was reached: albeit almost imperceptibly, sample mass was still declining at that point. Had the time-out point been set to a higher value, more gas may have desorbed at a given pressure, thereby decreasing, possibly eliminating the low-pressure hysteresis in the desorption isotherm.

Having said this, however, it should be noted that all the O<sub>2</sub> and N<sub>2</sub> isotherms obtained in the earlier work were determined using the same set of instrument operating parameters, including the value of the time-out point. Of particular note in this context is the fact that the corresponding isotherm in Figure 4 for O<sub>2</sub> adsorption on the CFCMS material is almost totally reversible, showing only a very small degree of hysteresis at the lowest pressures. Furthermore, all isotherms for N<sub>2</sub> and N<sub>2</sub> adsorption, respectively, on the CFCMS materials at the higher temperatures of 338 and 358K in the earlier work were fully reversible [8-10]. The salient point is that these observations indicated that the CFCMS material in question exhibited significant molecular sieving behavior between N<sub>2</sub> and O<sub>2</sub> at 294K. Because adsorption of N<sub>2</sub> on the CFCMS material took place in very small pores, possibly of dimensions approaching that of the N<sub>2</sub> molecule, it is a rate-controlled process with a positive temperature coefficient. When the temperature of the adsorption measurements was increased from 294 to 338K (and subsequently to 358K), the rate of diffusion of N<sub>2</sub> molecules into and out of the small pores increased

substantially and adsorption equilibrium was established within the time-out setting on the instrument, leading to fully reversible N<sub>2</sub> isotherms at the higher temperatures. Similar activated diffusion effects have been reported much earlier for N<sub>2</sub> adsorption on highly microporous activated carbons [15, 16].

Thus, the equilibrium uptake of O<sub>2</sub> on the CFCMS materials examined in the preliminary work exceeded that of N<sub>2</sub>, and there were clear indications that the low carbon burn-off (10%) material exhibited a strong molecular sieve effect. However, the differences between the equilibrium uptakes of N<sub>2</sub> and O<sub>2</sub> on the CFCMS material were small, and insufficient to indicate that the two molecules could be efficiently separated on the basis of their equilibrium adsorption behavior alone. Therefore, the work on the activated carbon fibers summarized here was carried out to provide the foundation for developing a suitable CFCMS material for air separation.

### 1.3.2 N<sub>2</sub> and CO<sub>2</sub> Adsorption Isotherm and Pore Size Distribution Data

The N<sub>2</sub> and CO<sub>2</sub> adsorption data obtained on the activated carbon fiber products are summarized in Table I.

Table 1 - Surface area and micropore volume data for activated carbon fiber products

Burn-off level (%)	5	10	15	20	30
N <sub>2</sub> BET area (m <sup>2</sup> g <sup>-1</sup> )	15	415	(790)	730	960
CO <sub>2</sub> BET area (m <sup>2</sup> g <sup>-1</sup> )	550	635	795	955	1170
Micropore volume (< 2 nm, DFT)	0.00	0.16	(0.32)	0.29	0.38
Micropore volume (< 2 nm, DA)	0.00	0.19	(0.33)	0.34	0.44

With the exception of the two values shown in parentheses, the N<sub>2</sub> and CO<sub>2</sub> adsorption data show the expected trends in the development of surface area and micropore volume (as measured by N<sub>2</sub> adsorption) with progressive increase in the degree of activation. It was noteworthy, however, that at the lowest burn-off level of 5%, a very pronounced molecular sieving effect was observed between N<sub>2</sub> and CO<sub>2</sub>. At 77K, nitrogen was unable to penetrate the ultrafine micropore structure developed under low burn-off conditions, resulting in an apparently very low BET surface area of 15 m<sup>2</sup>g<sup>-1</sup> and no measurable micropore volume. In contrast, carbon dioxide, at 273K, was able to enter the fine pores, revealing a significant surface area of 550 m<sup>2</sup>g<sup>-1</sup>. The flat molecular shape of CO<sub>2</sub> overcomes the slow diffusion or possible exclusion of N<sub>2</sub> molecules from the smallest pores at 77K, thus revealing details of the smallest micropores [17, 18].

As pore width increased with carbon burn-off, congruence was obtained between the N<sub>2</sub> and CO<sub>2</sub> data. This is illustrated graphically in Figure 5, in which representative isotherms for N<sub>2</sub> (at 77K) and CO<sub>2</sub> (at 273K) adsorption on the activated carbon fiber products are shown as composite plots (for the 5, 10, 20, and 30% burn-off levels, respectively). For the highest burn-

off level of 30%, the  $N_2$  and  $CO_2$  adsorption data essentially merge into the continuous type-I isotherm [19] shown in Figure 5d.

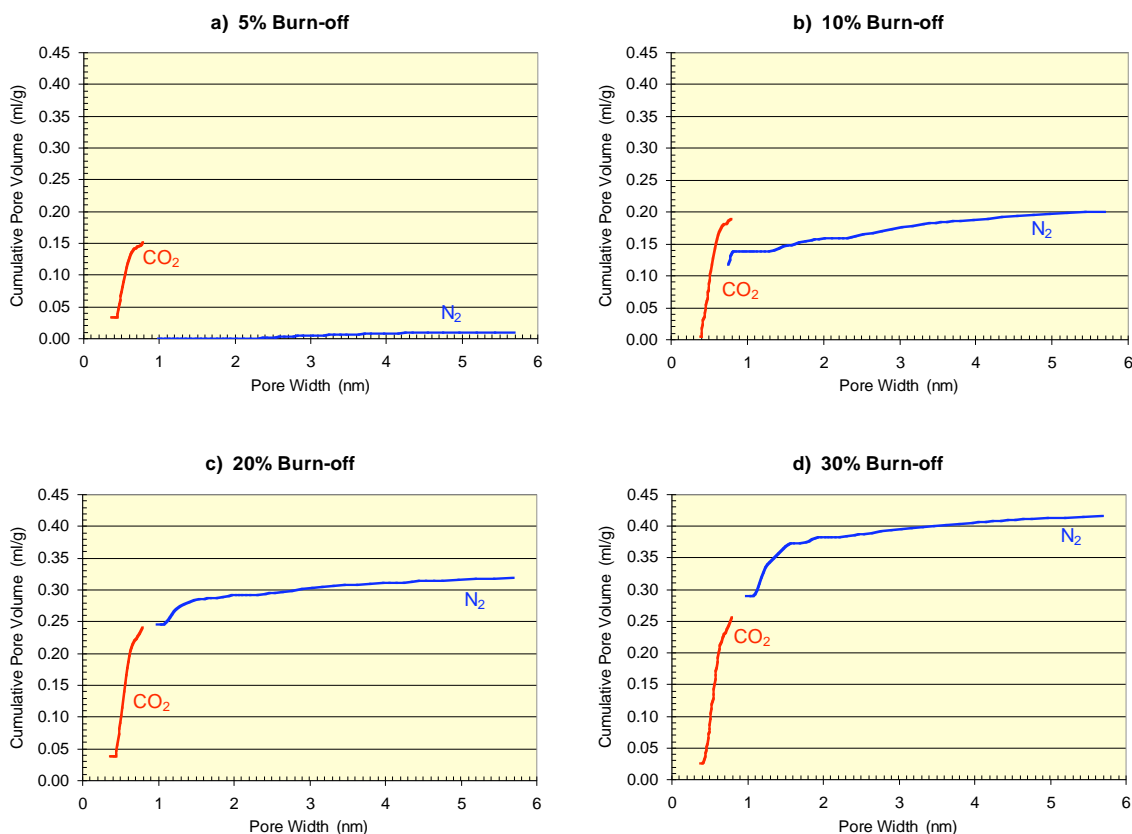


Figure 5 -  $N_2$  and  $CO_2$  adsorption isotherms as a function of carbon burn-off level

### 1.3.3 Dynamic $O_2$ and $N_2$ Adsorption Studies

The rates  $O_2$  and  $N_2$  adsorption, respectively, on the activated carbon fibers were measured at 294K. Each gas was dosed to the sample at two linear rates of pressure increase of 150 and 250 millibar/minute (0.015 and 0.025 MPa/minute), respectively, over the pressure range of 0.01-1 bar (0.001-0.1 MPa). Representative plots are shown in Figure 6 for gas uptake as a function of time (at the 150 millibar/minute dosage rate) for carbon burn-off levels of 5, 15, and 30%, respectively. The rates of  $O_2$  and  $N_2$  adsorption are summarized in Figure 7.

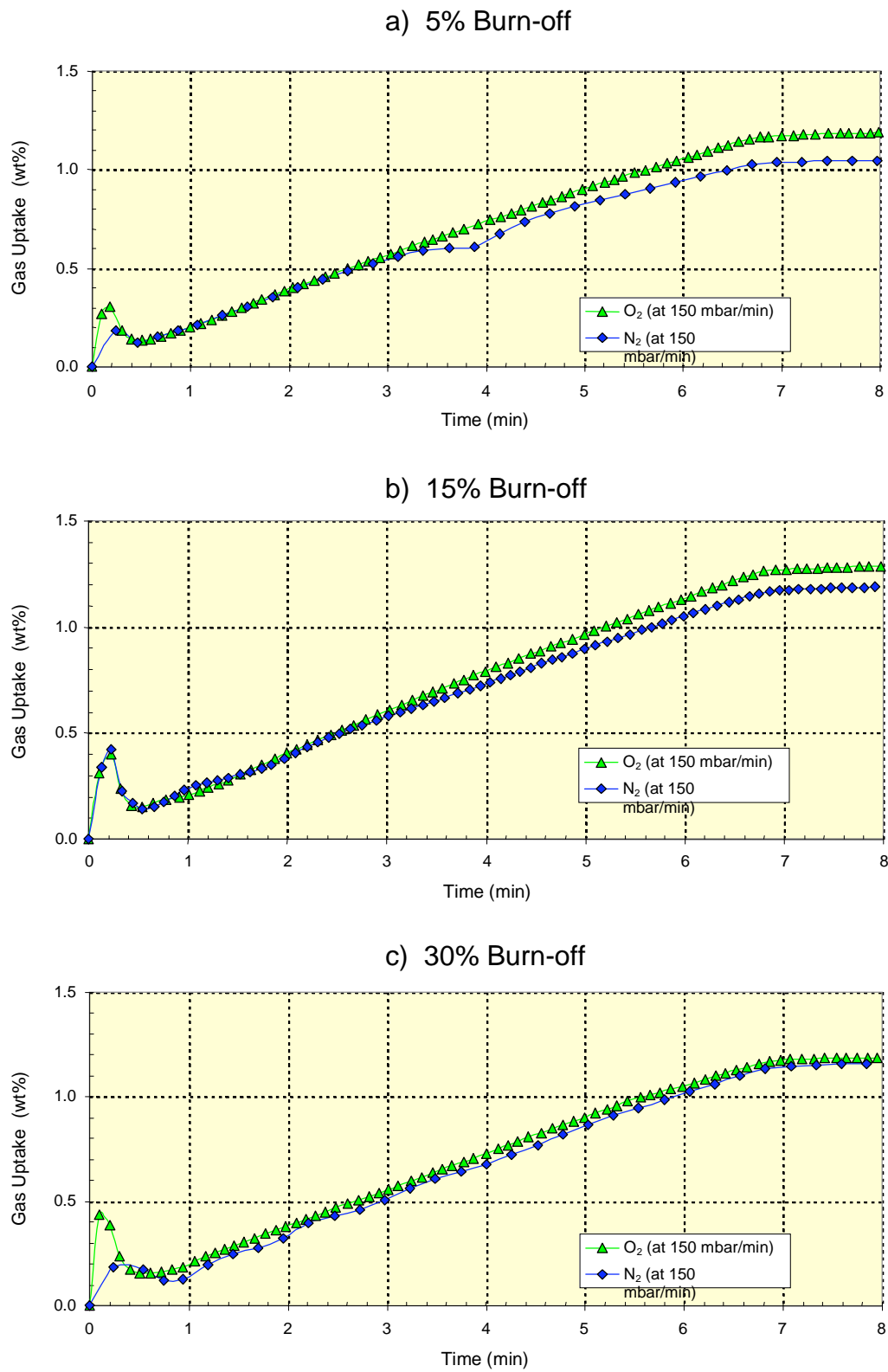


Figure 6 - Rates of O<sub>2</sub> and N<sub>2</sub> adsorption on activated carbon fiber products

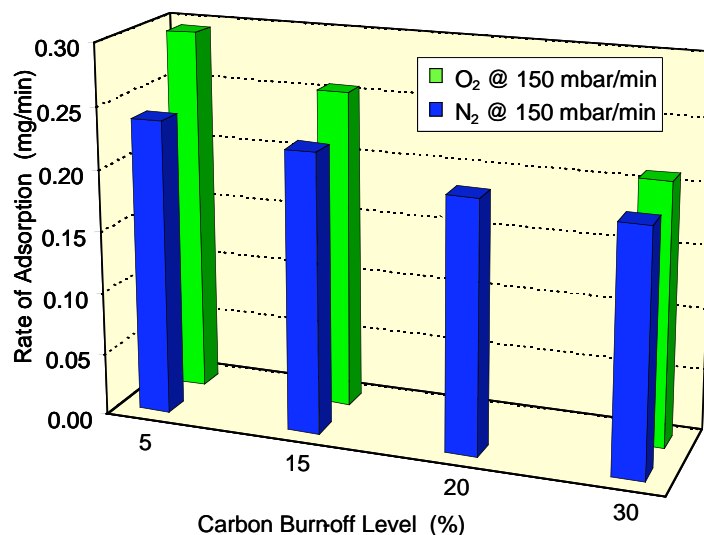


Figure 7 - Rates of O<sub>2</sub> and N<sub>2</sub> adsorption at 294K as a function of carbon burn-off level

It is apparent from Figures 6 and 7 that the rate of O<sub>2</sub> adsorption was markedly higher than that of N<sub>2</sub>, notably on the carbon fibers of lowest burn-off level of 5% (Figure 6a) which exhibited a 25% higher rate of O<sub>2</sub> adsorption (on a mass basis). The rate of adsorption of both O<sub>2</sub> and N<sub>2</sub> fell with progressive increase in the degree of activation of the carbon fibers. The amount of N<sub>2</sub> adsorbed at equilibrium at 1 bar (0.1 MPa) increased at the highest burn-off level of 30% (Figure 6b), indicative of the larger pore volume in this material. However, a consistent trend was not observed in the amount of either O<sub>2</sub> or N<sub>2</sub> adsorbed at equilibrium as a function of burn-off level, largely because the data for the 15% burn-off material (Figure 6b) indicated a higher adsorption capacity than expected. Coupled with the independent nitrogen adsorption isotherm data shown in parentheses in Table 1, this indicates that measured level of burn-off of the “15%” material may have been in error, and that it actually was substantially higher. Further work is necessary to resolve this question.

At both gas dosage rates, a sharp discontinuity was observed in the rate of N<sub>2</sub> adsorption on the 5% burn-off carbon at a pressure of about 0.045 MPa (corresponding to an elapsed time of about 3 minutes in Figure 6a). A similar change in rate of N<sub>2</sub> adsorption was observed for the 15% burn-off carbon, but to a lesser degree, and was not observed for the highest burn-off level of 30%. In contrast, a corresponding discontinuity in the rate of O<sub>2</sub> adsorption was not observed for any of the activated carbon fiber products. The reason for this (reproducible) discontinuity in the rate of adsorption of N<sub>2</sub> on the 5 and 15% burn-off carbon fiber products is not clear, but once again could be associated with a very pronounced molecular sieving effect in these materials. This observation is significant since the separation of O<sub>2</sub> and N<sub>2</sub> is a kinetic phenomenon, relying on the differences in the diffusion rates of the two molecules in narrow pore networks. The closer the pore width is to the molecular dimensions of the gasses the more significant the kinetic effects will be. Lower carbon burn-off level appears to be advantageous in this respect; higher levels (> 15%) increased micropore width to the point where molecular sieving effects were eliminated, which is counter-productive for air separation.



## 1.4 CONCLUSIONS AND FUTURE WORK

Data for the adsorption of  $O_2$ ,  $N_2$ , and  $CO_2$ , respectively, on isotropic pitch-based carbon fibers of varying degrees of activation demonstrated that a very low level of carbon burn-off is required to impart the molecular sieve properties in the carbon necessary for separation of  $O_2$  and  $N_2$  in air.  $O_2$  was more rapidly adsorbed on the activated carbon fiber than  $N_2$ , and with higher uptake under equilibrium conditions, providing the fiber contained a high proportion of very narrow micropores. The presence of the very narrow micropores in the low burn-off carbon fibers was revealed through the adsorption of  $CO_2$ , a more sensitive probe molecule than  $N_2$  for the presence of microporosity in adsorbents.

In addition to activation parameters, the adsorptive characteristics of activated carbon fibers are dependent on the nature of the precursor. In this context, lignin is a precursor known to produce highly microporous activated carbon products. In very preliminary work here, an activated carbon fiber was produced from a kraft hardwood, melt-spun lignin fiber. After stabilization and carbonization, the fiber was thermally-activated to a carbon burn-off level of 28%. Characterization of the pore size distribution properties of the activated carbon fiber is on-going, but the  $CO_2$  isotherms shown in Figure 8 illustrate the potential of lignin as a precursor for the production of a molecular sieving carbon fiber for air separation.

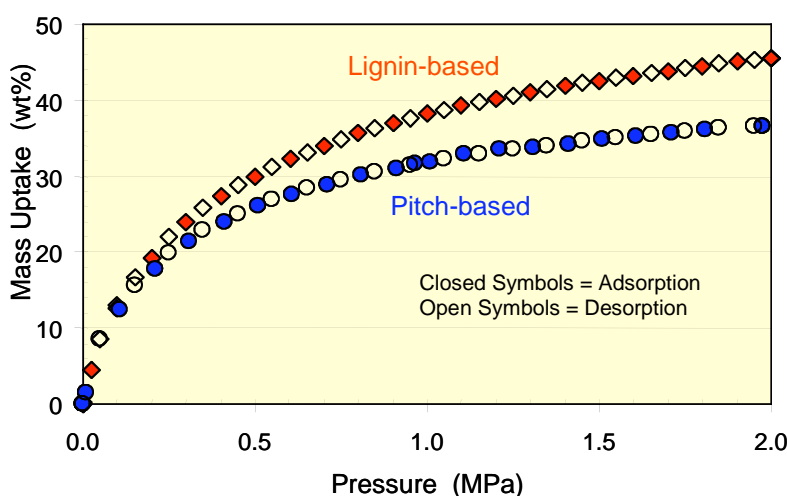


Figure 8 - Comparison of  $CO_2$  isotherms on lignin and pitch-based carbon fibers

The significantly higher  $CO_2$  adsorption capacity of the lignin-based activated carbon fiber is indicative of its more microporous structure compared to the pitch-based fiber of comparable burn-off level (30%). Furthermore, based on the findings reported here for the pitch-based fibers, an even more microporous carbon fiber should be obtained from a lignin precursor by activating it to a lower level of burn-off; e.g., 5-10%. Together with the examination of alternative activation techniques, this will be the subject of future work on the air separation project.

Overall, the findings reported here confirm that CFCMS has the potential for separating  $O_2$  and  $N_2$  from air on the basis of the different diffusion rates of the two molecules in the composite,

but the degree of separation is dependent on developing an extensive network of very narrow micropores in the activated carbon fiber. This in turn is dependent on identifying and demonstrating alternative techniques to obtain a uniform degree of activation throughout the bulk of the composite material, especially if a low level of carbon burn-off is the key to achieving the requisite micropore size distribution. In this context, it is essential to use a combination of molecular probes, such as CO<sub>2</sub> and N<sub>2</sub>, to properly characterize micropore size distribution.

To address engineering issues, a better understanding will be obtained of the factors that influence the permeability of CFCMS material, with the objective of reducing the pressure drop of the material for air separation and other applications. Similarly, alternative activated carbon composite forms will be evaluated, including honeycombs. Activated carbon honeycombs are used commercially for demanding gas phase applications, including capture of trace amounts of fugitive gasoline emissions from vehicles. The incorporation of highly microporous carbon fibers into such honeycombs has not been reported, however, and may have the potential of producing a very low pressure drop form that exhibits greater capacity and efficiency for air separation.

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